Ancient Monuments Laboratory Report 39/96

THE EXAMINATION OF METALWORKING DEBRIS FROM HOUSESTEADS ROMAN FORT, NORTHUMBERLAND 1974-1981

D Starley

AML reports are interim reports which make available the results of specialist investigations in advance of full publication. They are not subject to external refereeing and their conclusions may sometimes have to be modified in the light of archaeological information that was not available at the time of the investigation. Readers are therefore asked to consult the author before citing the report in any publication and to consult the final excavation report when available.

Opinions expressed in AML reports are those of the author and are not necessarily those of the Historic Buildings and Monuments Commission for England.

## Ancient Monuments Laboratory Report 39/96

## THE EXAMINATION OF METALWORKING DEBRIS FROM HOUSESTEADS ROMAN FORT, NORTHUMBERLAND 1974-1981

D Starley

 $\bar{\mathbf{a}}$ 

### Summary

A small quantity of debris recovered from excavations in the north-east corner of the fort derived from both iron smithing and a wider range of non-ferrous alloy working. Some slag provided rare unambiguous evidence for the use of coal in Romano-British ironworking.

 $\hat{\mathcal{L}}$ 

Author's address :-

Dr D Starley ENGLISH HERITAGE 23 Savile Row London W1X lAB

© Historic Buildings and Monuments Commission for England

#### ANCIENT MONUMENTS LABORATORY REPORTS SERIES

# **The examination of metalworking debris from Housesteads Roman Fort, Northumberland 1974-1981**

David Starley

## Introduction

 $\mathcal{B}$ 

Excavations at Housesteads fort (NY 790688) between 1974 & 1981 investigated the north-east corner of the fort, focusing principally on barrack block XIII, the adjacent rampart back and the intervallum roadway areas from the north gate to the north-east angle tower and thence to the east gate'. The project served as a training dig for second year students at the Department of Archaeology in the University of Newcastle upon Tyne. Outside these intensive 3 week spells, excavation was continued by smaller numbers of volunteers. Between 1974 and 1977, the excavations were directed by C.M. Daniels and J.P. Gillam with J.G. Crow joining the team as assistant director from 1978. An industrial area was identified behind the ramparts, this included a number of large hearths of uncertain purpose.

Only small areas of the site were opened at any time, with excavation proceeding sequentially each season. The site/building codes derive from the numbering sequence of R.C. Bosanquet following trial trenching in 1898. The sequence of excavation was as follows:

- 1974-77 Complete exploration of building XIII (HI3)
- 1977 Exploratory trench opened in the north rampart area. Building XIII excavation extended across the north end of the *via principalis,* revealing the east end of building  $VII$  ( $H13:11$ ).
- 1977-78 Clearance down to the upper most road surface of the street between buildings XIII and XIV.
- 1978-79 North rampart back and roadway area- north gate to north-east angle tower (H20).
- 1979 Examination of the western-most contubernium/chalet of building XIV (H14:9).
- 1980-81 East rampart back and roadway area north-east angle tower to east gate (H21).
- 1981 Re-examination of the east end of building XV where a bath-house was inserted during the fourth century (first investigated by Wilkes in 1961) (H15:1).
	- The east end of the road between XIII and XIV excavated down to a suitable level for display (HSE)
	- Re-examination of the remains of building XIV, first excavated by Wilkes in 1961 (HI4:I,3-6).

## Site Phasing

 $\mathcal{A}^{\mathcal{A}}$  $\ddot{r}$ 

> A short pre-fort phase was identified in site H20. The fort itself can be divided into four phases:



To some extent phasing within the separate areas of excavation "float" with respect to other areas. Phasing codes used in the context lists follow the scheme of Mike Bishop (1989):





 $\sim 100$ 

 $\sim$ 

## Table 2 Metalworking debris from Housesteads



 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2.$ 

 $\mathcal{L}^{\text{max}}_{\text{max}}$ 









 $\mathcal{A}^{\mathcal{A}}$ 

 $\sim 10^{-1}$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\left(\frac{1}{\sqrt{2}}\right)^2\frac{1}{\sqrt{2}}\frac{1}{\sqrt{2}}\frac{1}{\sqrt{2}}\frac{1}{\sqrt{2}}\frac{1}{\sqrt{2}}\frac{1}{\sqrt{2}}$ 

 $\label{eq:2.1} \frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1}{\sqrt{2\pi}}\int_{\mathbb{R}^3}\frac{1$ 

 $\sim$ 





 $\sim 10^7$ 





## Assessment of the metalworking debris

 $\ddot{\phantom{a}}$ 

l,

This involved the visual examination of all slags and metalworking debris retrieved from the site. The bulk slag totalled 24kg and this has been classified and quantified in Table 2 and summarised in Table 3.



Visual examination of metalworking debris allowed the material to be categorised on criteria of morphology, density, colour and vesicularity. It should be stressed that many "classes" of iron working slags form part of a compositional and morphological continuum. Only certain classes of material are strictly diagnostic, and can **be**  unambiguously assigned to a single metalworking process. Others may derive from a restricted range of processes but, when found in association with the diagnostic types may provide support for these activities. Some forms of debris may originate from a very wide range of high temperature processes and are of no help in identifying crafts or industries. Class names and the criteria on which they are based may vary between specialists. Those currently used by the Ancient Monuments Laboratory are defined below.

## Explanation of classification

Evidence for the smithing *(i.e.* hot working) of iron comes in two main forms; bulk slags and micro slags. Of the bulk slags produced during smithing only the **smithing**  hearth bottoms are unlikely to be confused with the waste products of smelting and are therefore considered to be diagnostic of smithing. These hearth bottoms are recognisable by their characteristic plano-convex form; typically having a rough convex base and a smoother, vitrified, upper surface which is flat, or even slightly hollowed as a result of the downwards pressure of the air blast from the tuyere. Compositionally, smithing hearth bottoms are predominantly fayalitic (iron silicate) and form as a result of high temperature reactions between the iron, iron-scale and silica from either the clay furnace lining or sand used as a flux by the smith.



Twenty examples of smithing hearth bottoms were identified in the material from Housesteads. The statistics of this group, given in Table 3, show a very wide range of sizes. However, many examples were very small and the mean weight figures are unusually low for this (or any other) period. The Housesteads smithing hearth bottoms are also notable because they comprise a large proportion of the total weight of slag examined. By comparison with Roman debris from other sites they were also dense and well-consolidated, rather than the typically more cindery residues.

In addition to bulk slags, iron smithing also produces micro-slags of two types. Flake hammerscale consists of fish-scale like fragments of the oxide/silicate skin of the iron dislodged during working. Spheroidal hammerscale results from the solidification of small droplets of liquid slag expelled during working, particularly when two components are being fire welded together or when a slag-rich bloom of iron is first worked into a billet or bar. Hammerscale is considered important in interpreting a site not only because it is highly diagnostic of smithing but, because it is often allowed to build up in the immediate vicinity of the smithing hearth and anvil, it may give a more precise location of the activity than the bulk slags which may be transported elsewhere for disposal<sup>2</sup>. During the visual examination of bulk slags, small quantities of hammerscale, almost exclusively of the flake variety, were identified in bags from nine different contexts. This information has been noted in Table 2, but without quantification.

Evidence for the smelting of iron *i.e.* the primary extraction of the metal from an ore was restricted to two fragments of very glassy material. One of these was analysed by X-ray fluorescence to confirm its identification. Such slags are not totally unknown from Roman iron smelting assemblages but, because they form only a very small component of the assemblage, they are explained as an unintentional product caused by excessive air supply in the presence of calcium-rich material. No raw materials or waste products typical of Roman iron smelting technology was identified. The latter would include the dense, fayalitic slags known as tap slags which show a ropy flowed structure on their upper surface and little porosity. It must be assumed that iron smelting was not carried out on the site and the material present is intrusive blast fumace slag, possibly deriving from recent, local use of the material as hardcore.

Ferruginous concretion forms as a result of the redeposition of iron hydroxides, similar to the natural phenomenon of iron panning, although the process is likely to be enhanced by the nature of the surrounding archaeological deposits, particularly iron-rich waste. The largest piece of this material examined, from H20, Area 7, Context 75 contained flakes of hammerscale and provides further evidence of iron smithing.

Amongst the large quantity of iron objects found within the debris several may provide direct evidence of ironworking on site. Two pieces of what appeared to be the cut off ends of bar stock were recovered. The first fragment from H20, Area2, Context 4 measured 40x8mm in section and had been cut down to a length of 25mm. A second piece from the topsoil of H20, Area 5 of 50x20mm section was 70mm long.

Evidence for further metalworking activities, the casting and working of copper alloys was recognised in a number of forms. The largest category by weight was slag with copper corrosion products. Apart from the bright green copper oxides on the surface, this material does not differ greatly from that produced during iron smithing, often having a dense fayalitic structure. This would not be the waste product expected from purely melting and casting activities and may be indicative of hot working of copper alloys and iron in the same hearth. Unambiguous evidence of copper alloy melting and casting was provided by crucible and mould fragments. The former were present in a wide range of forms; both wheel thrown and hand moulded, coarse and fine fabrics and with and without the top crimped to a triangular opening. Many examples showed black or red glazes externally, the latter being a clear indicator of the presence of copper, whilst fewer had copper corrosion products attached. The two mould fragments were too small to identify the artefacts which were being cast from them.

l,

Large quantities of copper alloy waste were included within the assemblage. These included amorphously shaped pieces described as drips, blobs and spills. In the context of the materials described above these are most likely to be waste products of casting although it is possible that copper artefacts, accidentally caught in a conflagration, could take a similar form. Offcuts took a limited range of forms most common were small trimmed fragments of very thin sheet, but small bars with tapered down ends were also present showing that copper artefacts were wrought as well as cast.

Lead, or as suggested by the very advanced corrosion, pewter was also identified. It is possible that this may have resulted from some manufacturing process. Unfortunately, the low temperatures required for the melting of lead alloys do not normally result in the formation of robust slags. With only three examples of the metal, it is thought that lead working, if it occurred at all, was not carried out on a significant scale on the site.

Four categories not considered diagnostic are undiagnostic ironworking slag, vitrified hearth lining, cinder and iron-rich cinder. However, in the absence of clear evidence for iron smelting on the site it is probable that most of the denser material within these three categories derives from iron smithing, although some of the lighter cindery material and the hearth lining material may be associated with non-ferrous alloy working and this is attested by occasional bright red glazes on hearth lining. Slags classed as undiagnostic ironworking slags are predominantly fayalitic, but their morphology is irregular and similar materials may be produced by smelting and smithing operations. Vitrified hearth/furnace lining can form during either iron smelting, iron smithing or non-ferrous metal working as a result of a high temperature reaction between the clay lining of the hearth/furnace and the alkali fuel ashes or fayalitic slag. The material may show a compositional gradient from unmodified clay on one surface to an irregular cindery material on the other. An associated material, classed as cinder, comprises only the lighter portion of this, a porous, hard and brittle slag formed as a result of high temperature reactions between the alkali fuel ashes and either fragments of clay which had spalled away from the hearth/furnace lining or another source of silica, such as the sand used as a flux during smithing. Iron-rich cinder is a porous material but contains a significant iron content. A large bag (not weighed) of oxidised fired (red) lining from a hearth (Context 63, Area 5, H20) was of a crumbly nature. It provided no clues for the purpose of the hearth.

Fuels and their residues form a separate group of material. As well as a few examples of charcoal, fragments of coal were found from numerous contexts. Whilst a number of Romano British sites have provided evidence to link the use of coal to metallurgical processes, the extent and exact purposes to which the fuel was used remain unclear'.

Many early reports are based on unsound assumptions as to the nature of the metalworking activity. Unambiguous evidence linking the fuel to diagnostic debris is rare and the smithing hearth bottom containing coal fragments from Phase4 of Site21, Area2, Context 18 provides an unusually powerful link. The fuel ash slag, ashy deposit, fired clay and bumt stone may result from a number of high temperature processes and cannot be assumed to originate from metallurgical processes.

### Conclusions

Although the quantities of debris recovered from the excavations of Housesteads Fort were modest, they represented a broad range of metallurgical activities. Iron smithing was represented by smithing hearth bottoms, hammerscale and bar ends, whilst nonferrous alloy working had left crucibles and mould fragments from casting as well as offcuts indicating the working of sheet and bar. There is no evidence of iron smelting on site and insufficient material to more than suggest the possibility of the working of lead or other lead-based alloys.

At the time of examination phasing for the site was provisional, with some uncertainty over continuity between the separate sites. A brief examination of the data did not point to any particularly intense period of metalworking activity. Non-ferrous debris is associated with all phases from the primary construction of the fort onwards. Iron smithing, surprisingly, appears more restricted with no firm evidence during the construction phase and only limited material in Phase II, restricted to H20. Iron working debris becomes more common in the later phases and a large proportion of the smithing hearth bottoms were from topsoil contexts, perhaps because they are easily recognised even during rapid removal of overlying deposits.

The excavation of the north and east rampart provided 75 % of the weighed slag in the assemblage, and a further large bag of furnace lining from the north rampart, H20, was unweighed. This material, together with most other reported to be from hearths in this area, provided no finn evidence with which to link the structures to metalworking activity. However, hearth 75 (H20, Area7) did contain both hammerscale and nonferrous debris suggesting iron smithing at least in the immediate vicinity. It should be noted that elsewhere the comparative rarity of archaeologically surviving smithing hearths has led to the assumption (supported by graphic evidence) that most smithing hearths were built into raised platforms for ease of working.

Assessing the importance of metalworking at Housesteads is problematic. On the one hand such limited quantities of debris may bear witness only to small scale or short term working of iron. However, the relatively dispersed nature of the evidence, by area and period, suggests much larger scale of activity but with the majority of bulk debris not being deposited in the immediate area of activity.

## Potential for further work

Despite the relatively small size of the debris assemblage, its greatest potential lies in the wide range of material available for study. Recognition of iron bar stock on a smithing site and unambiguous linking of smithing with the use of coal are rare occurrences. Unfortunately, such limited quantities of material would restrict any conclusions that might be drawn. Thus the material might be more appropriate for a wider study, such as one that compared it with similar assemblages from other sites, perhaps as a student project.

The non-ferrous assemblage certainly deserves more detailed study than the time available within this assessment. Again, the importance of the assemblage lies in its wide range of materials. Such a study would include detailed examination of the crucible fragments by a specialist in that subject, together with non-quantitative analysis of metallurgical residues attached to the crucibles. This material should then be compared with analyses of copper alloy waste and artefacts from the site, to provide a basis on which to understand the range and significance of the copper alloy working within the fort at Housesteads.

## Storage of slag

Slag, being predominantly fayalitic, is not prone to deterioration and requires no special storage treatment. Crucible fragments are relatively stable and may be stored as ceramics, unless they also contain significant metallic residues. Mould fragments are normally unfired, are relatively fragile and require protection from physical attrition. All iron, copper alloy and lead alloy objects should be removed and stored under more appropriate conditions. It is recommended that all debris should be saved.

#### References

I. Information on site background, contexts and phasing provided by Alan Rushworth: Housesteads Project Slag Analysis: Background Information and Context Lists, February 1996.

2.Mills, A. and McDonnell, JG. The Identification and Analysis of the Hammerscale from Burton Dasset, Warwickshire, Ancient Monuments Laboratory Report 47/92.

3. Dearne, Martin J. and Branigan, Keith. The Use of Coal in Roman Britain, Antiquaries Journal, 75,1995, pp71-105.